

Microwave Absorption Properties of Garnet Ferrite Filled Polymer Nanocomposites in X-Band

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Abstract. The electromagnetic properties of ferrite filled polymer nano-composites can be determined by a classical Nicolson-Ross and Weir technique. The measurement of S-parameters makes it possible to calculate the complex permittivity ϵ and permeability μ of the Lanthanum Iron Garnet (LIG)-loaded polyvinylidene fluoride (PVDF)-polymer nanocomposites over the X-band waveguide. The reflection S_{11} and transmission S_{21} coefficients were calculated by the transmission/reflection rectangular waveguide technique. The LIG/PVDF sample, placed in the rectangular waveguide over X-band frequencies. The average values of the relative complex permittivity and permeability of LIG/PVDF over X-band frequencies [8 - 12 GHz] are $(4.34 - j0.09)$ and $(1.27 - j0.15)$ respectively.

Keywords: Complex permittivity and permeability, Ferrite, Garnet, LIG, PVDF, waveguide W-90, X-band.

1 Introduction

Ferrites are ferrimagnetic oxides materials have been heavily used in passive microwave devices such as circulators, isolators, phase shifters, resonators, filters, and miniature antennas [1]. The garnets are soft ferrites having the general chemical formula $R_3Fe_5O_{12}$ where R is yttrium or trivalent rare earth ions from lanthanum to ytterbium[2]. Garnet ferrites have a cubic crystal structure and include three types of crystallographic lattice of (a,b and c), the $3R^{3+}$ ions are located the dodecahedra (c) site, $2Fe^{2+}$ ions are distributed to the octahedral (a) site and $3Fe^{3+}$ ions occupying the tetrahedral (d) site, where as O^{2-} ions are located to the interstitial sites [3].

Lanthanum Iron Garnet (LIG) has a chemical formula $La_3Fe_5O_{12}$, it is strongly used in electronic devices, due to the efficient absorption of electromagnetic waves, low permeability, low losses at high frequencies, extremely easy to magnetize and demagnetize, low saturation flux, and high resistivity. In recent years, many works have been made on polymer matrix - based nanocomposites filled with ferrite particles, such as Co-ferrite [4], Ni-Zn-ferrite [5], and Mn-Zn-ferrite [6], using different characterization methods [7].

In this paper, the transmission/reflection (TR) characterization method based on Nicolson-Ross-Weir approach allows to calculate simultaneously the complex relative permittivity and complex relative permeability of the lanthanum iron garnet filled -PVDF polymer nanocomposite, from the S-parameters, the sample was placed in a rectangular waveguide over the X-band frequencies [8 – 12 GHz], and with the ANSYS HFSS simulation, we can

measure the reflection and transmission coefficients and calculate the complex relative permittivity and complex relative permeability of LIG/PVDF composites.

2 Materials and methods

Many papers for the physico-chemical synthesis of lanthanum iron garnet have been described in [8,9] by sol-gel procedure.

2.1 Preparation of the LIG powder

The procedure for preparing LIG magnetic powders is shown in the diagram below. **Figure 1.**

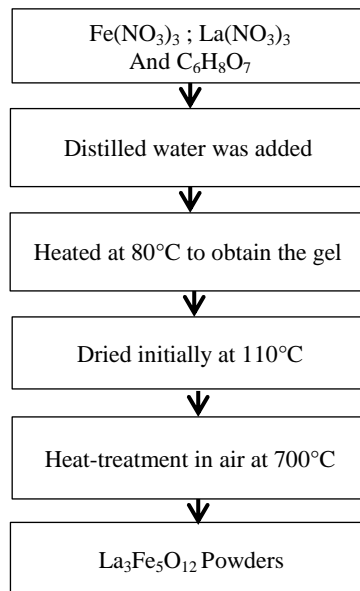


Fig. 1. Procedure for preparing Lanthanum Iron Garnet powders

The LIG/PVDF as a nanocomposite was prepared by the solvent method , with 13% LIG nano-powders and 87% of PVDF polymer in the shape of a rectangular sheet 3 mm thickness.

2.2 Simulation of the rectangular waveguide loaded with the sample LIG/PVDF

The PVDF-LIG nano-composite sample of dimensions (22.86*11.43*3mm³), was well adjusted into a rectangular waveguide cross section WR-90. The S-parameters then were measured in the frequency range from 8 to 12 GHz by using the HFSS simulator. The simulation can be shown in **Figure 2**.

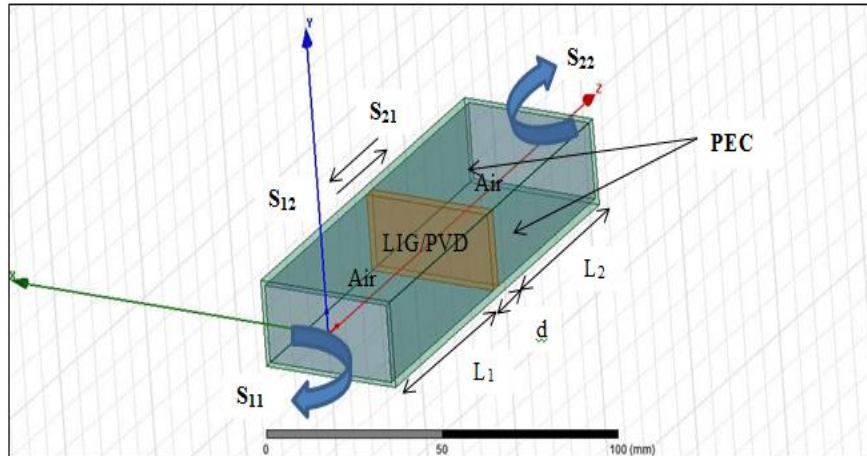


Fig. 2. Simulation of the rectangular waveguide

2.3 Nicholson-Ross-Weir (NRW) method

Determination of the electromagnetic properties of PVDF-LIG composite sample using transmission/reflection rectangular waveguide technique[10-12]. The organigram shown in the **Figure 3** describes the procedure for extracting the S-parameters and estimation complex permeability and permittivity of the sample under study.

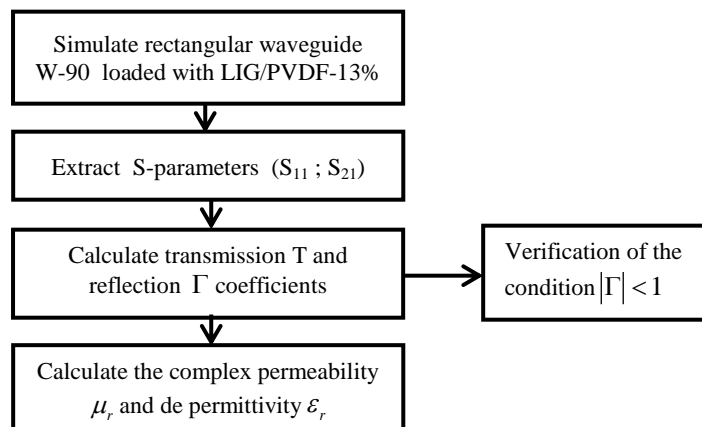


Fig. 3. Algorithm of Nicolson-Ross and Weir

The proposed classical procedure by Nicolson-Ross and Weir is based on the following formulas, these equations are applicable for the rectangular waveguide with the transverse electric TE₁₀ mode.

$$S_{11} = R_1^2 \frac{\Gamma(1-T^2)}{1-\Gamma^2 T^2} \quad (1)$$

$$S_{21} = R_1 \times R_2 \frac{T(1-\Gamma^2)}{1-\Gamma^2 T^2} \quad (2)$$

$$R_1 = \exp(-\gamma_0 L_1) \quad \text{and} \quad R_2 = \exp(-\gamma_0 L_2) \quad (3)$$

$$T = \exp(-\gamma d) \quad (4)$$

$$\gamma = j \frac{2\pi}{\lambda_0} \sqrt{\epsilon_r \mu_r - \left(\frac{\lambda_0}{\lambda_c}\right)^2} \quad (5)$$

$$\gamma_0 = j \frac{2\pi}{\lambda_0} \sqrt{1 - \left(\frac{\lambda_0}{\lambda_c}\right)^2} \quad (6)$$

$$\Gamma = K \pm \sqrt{K^2 - 1} \quad (7)$$

$$K = \frac{S_{11}^2 - S_{21}^2 + 1}{2S_{11}} \quad (8)$$

$$T = \frac{S_{11} + S_{21} - \Gamma}{1 - (S_{11} + S_{21})\Gamma} \quad (9)$$

$$\mu_r = j \left(\frac{1+\Gamma}{1-\Gamma} \right) \times \frac{c}{2\pi fd} \ln(T) \quad (10)$$

$$\epsilon_r = - \left(\frac{c}{2\pi fd} \ln(T) \right)^2 \times \frac{1}{\mu_r} \quad (11)$$

- Γ and T are respectively the reflection and transmission coefficients;
- γ_0 and γ are respectively the propagation constants in the vacuum and sample;
- λ_0 and λ_c represent respectively the free space and the cut-off wavelengths;
- ϵ_r et μ_r are the relative permittivity and permeability respectively.
- R_1 and R_2 correspond the expression of reference planes respectively.
- L_1 and L_2 are the respective distances from calibration reference planes to sample ends.
- d is wavelength of sample.

3 Results and discussion

The Nicolson-Ross and Weir (NRW) technique was used to calculate the complex permittivity and permeability of LIG/PVDF nanocomposite, from reflection S_{11} and transmission S_{21} coefficients using the transmission/reflection (TR) measurement technique. **Figure 4a.** below shows two response the curves of LIG/PVDF sample of the real permittivity and imaginary permittivity as function of frequency. The real part of permittivity is decreasing from 8GHz to 12GHz, this real part has a high value nearly 6.08 in frequency at 8GHz, and then decreases to 3.45 at 12GHz when the frequency increases. This figure also represents the imaginary part of the permittivity curve. The imaginary part has a small variation with frequency increases from 8GHz to 12GHz. The observed response of the permittivity constant is the result of adding the portion of the LIG magnetic in PVDF polymer matrix [13].

The **Figure 4b.** below, presents two response the curves of LIG/PVDF nanocomposite of the real permeability and imaginary permeability as function of frequency. it illustrates that the real part of permeability is 3.53 at 8GHz, from this point, the curve of the real permeability shows a gradual decrease with increasing frequency to reach 0.23 at 12 GHz.

Similarly, the imaginary part decreases from 0.75 to 0.01 with increasing frequency from 8GHz to 12GHz, the decreasing is the product of the domain wall motion and the spine-lattice interaction.

The average values obtained in this work of the complex permittivity and permeability respectively of mentioned above nanocomposite in X-band frequencies were $(4.34-j0.09)$ and $(1.27-j0.15)$. The results achieved in this project are in excellent agreement with the literature[14].

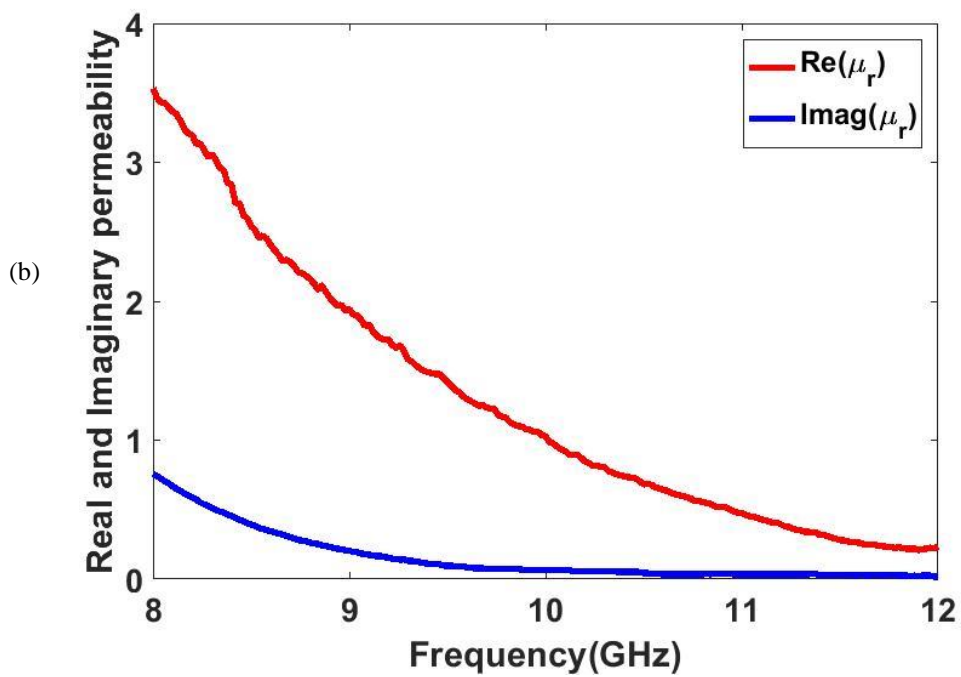
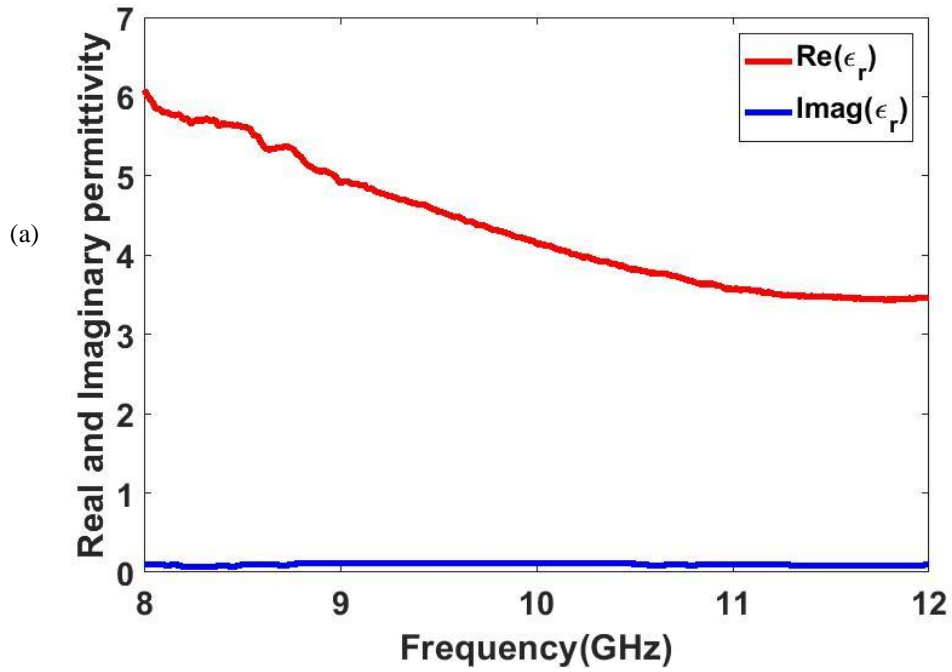


Fig. 4. Evolution of (a) Complex permittivity and (b) Complex permeability of LIG/PVDF nanocomposite versus frequency

Table 1. below represents the comparison between the values calculated and measured [14].

Table 1. Comparison table between the calculated parameters and the measured parameters

LIG/PVDF-13%	ϵ_r	μ_r	Error $\frac{\Delta\epsilon_r'}{\epsilon_r'}$	Error $\frac{\Delta\mu_r'}{\mu_r'}$
Calculated	4.34-j0.09	1.27-j0.15	$\leq 0.23\%$	$\leq 2.3\%$
Measured	4.33-j0.09	1.24-j0.15		

Conclusions and perspectives

In this paper, the LIG/PVDF nanocomposite has been fabricated in the shape of rectangular sheets with thickness of 3mm. The S-parameters were measured by the cross section rectangular waveguide at the X-band. The Nicholson-Ross-Weir (NRW) procedure was employed to calculate the complex permittivity and complex permeability of the LIG/PVDF sample. The results indicated at X-band frequencies, show the both real part of permittivity, real part of permeability and imaginary part of complex permeability are decreased when increasing the frequency in X-band. But, the imaginary part of the dielectric permittivity probably remains constant in this frequency range. The average values obtained in this work of the complex permittivity and permeability respectively of mentioned above nanocomposite in X-band frequencies were (4.34-j0.09) and (1.27-j0.15). The results achieved in this project are in excellent agreement with the literature[14].

Acknowledgement

The authors would like to thank the members of Institute of Electronics and Telecommunications of Rennes, France for allowing us to use the commercial solvers available in their laboratory.

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